

# Terminology: Lagrangean, Eulerian descriptions

When  $\underline{r}_0$  at time 0 moves to  $\underline{r}$  at time  $t$  and

$$f(\underline{r}(\underline{r}_0, t), t) = f_L(\underline{r}_0, t)$$

the **material time derivative** is

$$\frac{D}{Dt} f(\underline{r}, t) = \frac{\partial}{\partial t} f_L(\underline{r}_0, t) = \frac{\partial f}{\partial t} + \underline{q} \cdot \nabla f$$

where  $\underline{q} = \underline{q}(\underline{r}, t)$  is the velocity. Here  $f_L$  is the Lagrangean description and  $f$  is the Eulerian description.

Applying this to  $u$ ,  $v$  and  $w$  in  $\underline{q} = u \underline{i} + v \underline{j} + w \underline{k}$  gives

$$(\text{Lagrangean acc}) = (\text{Local acc}) + (\text{Convective acc})$$

$$\underline{a}_L = \frac{D}{Dt} \underline{q} = \frac{\partial \underline{q}}{\partial t} + (\underline{q} \cdot \nabla) \underline{q}.$$

# Terminology describing fluid flows

$$\underline{r} = x\underline{i} + y\underline{j} + z\underline{k}, \quad \underline{q} = \underline{q}(\underline{r}, t) = u\underline{i} + v\underline{j} + w\underline{k}.$$

**Two-dimensional flow in  $x, y$  plane:**

$$w = 0 \quad \text{and} \quad \frac{\partial u}{\partial z} = \frac{\partial v}{\partial z} = \frac{\partial \rho}{\partial z} = 0.$$

**Steady flow:**

$$\frac{\partial \rho}{\partial t} = 0 \quad \text{and} \quad \frac{\partial \underline{q}}{\partial t} = 0.$$

**Stagnation Point:** This is a point at which  $\underline{q} = \underline{0}$  for all time.

**Particle Paths:** From a Eulerian description we have

$$\frac{d\underline{r}}{dt} = \underline{q}(\underline{r}, t), \quad \text{with } \underline{r}(0) = \underline{r}_0.$$

**Streamlines:**

$$x(s)\underline{i} + y(s)\underline{j} + z(s)\underline{k} \quad \text{where} \quad \frac{x'(s)}{u} = \frac{y'(s)}{v} = \frac{z'(s)}{w}.$$

Streamlines are the same as particle paths when the flow is steady.

## Example

2D unsteady flow described in Eulerian form by

$$\underline{q}(\underline{r}, t) = \underline{q}_E(\underline{r}, t) = xt \underline{i} - y \underline{j}, \quad t \geq 0.$$

Particle paths satisfy

$$\begin{aligned} \frac{dx}{dt} &= u = xt, \\ \frac{dy}{dt} &= v = -y. \end{aligned}$$

Streamlines at fixed time  $t$  satisfy

$$\frac{dx}{u} = \frac{dy}{v} \quad \text{i.e.} \quad \frac{dx}{xt} = \frac{dy}{-y}$$

## Example

2D unsteady flow described in Eulerian form by

$$\underline{q} = U \underline{i} + \frac{x}{(1+t)} \underline{j}, \quad t \geq 0,$$

Particle paths satisfy

$$\begin{aligned} \frac{dx}{dt} &= u = U, \\ \frac{dy}{dt} &= \frac{x}{1+t}. \end{aligned}$$

Specifying an initial condition  $x(0) = x_0$ ,  $y(0) = y_0$  gives a particular path.

Streamlines at fixed time  $t$  satisfy

$$\frac{dx}{u} = \frac{dy}{v} \quad \text{i.e.} \quad \frac{dx}{U} = \frac{dy}{\left(\frac{x}{1+t}\right)}.$$

## Equation of mass conservation and incompressibility

For a region  $\Omega$  without sources and sinks the change in the amount of mass in  $\Omega$  is entirely encountered for by the flow of the material through the surface  $S$  of  $\Omega$  and this leads to

$$\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho \underline{q}) = 0$$

or equivalently

$$\frac{D\rho}{Dt} + \rho \nabla \cdot \underline{q} = 0.$$

A material is **incompressible** if

$$\frac{D\rho}{Dt} = 0 \quad \text{which is equivalent to} \quad \nabla \cdot \underline{q} = 0.$$

## Equation of hydrostatic pressure

Let  $\Omega$  be an region with surface  $S$ . In equilibrium

$$(\text{force on surface}) + (\text{force due to gravity}) = \underline{0}$$

## Euler's equations of motion

(force due to acc.) + (force on surface) + (force due to gravity) =  $\underline{0}$ .

$$\rho \frac{D\mathbf{q}}{Dt} = -\nabla(p + \rho gz).$$

With steady flow

$$\frac{D\mathbf{q}}{Dt} = (\mathbf{q} \cdot \nabla)\mathbf{q} = \nabla \left( \frac{1}{2} |\mathbf{q}|^2 \right) + (\nabla \times \mathbf{q}) \times \mathbf{q}.$$

The term

$$\underline{\omega} = \nabla \times \mathbf{q}$$

is known as the vorticity. We can connect the velocity  $\mathbf{q}$  with the pressure  $p$  along streamlines. With several 2D flows  $\underline{\omega} = \underline{0}$ .

## Further comments relating to Euler's equations

When the fluid is incompressible the density  $\rho$  is constant.

Steady incompressible flow thus involves

$$\rho \frac{D\underline{q}}{Dt} = \rho(\underline{q} \cdot \nabla)\underline{q} = -\nabla(p + \rho gz).$$

Using the identity gives

$$\rho \nabla \left( \frac{1}{2} |\underline{q}|^2 \right) + \rho (\nabla \times \underline{q}) \times \underline{q} = -\nabla(p + \rho gz).$$

i.e.

$$\nabla \left( \frac{1}{2} |\underline{q}|^2 + \frac{p}{\rho} + gz \right) + (\nabla \times \underline{q}) \times \underline{q} = \underline{0}.$$

On a streamline

$$H = \frac{1}{2} |\underline{q}|^2 + \frac{p}{\rho} + gz$$

is a constant.  $H$  is constant everywhere when  $\underline{\omega} = \nabla \times \underline{q} = \underline{0}$ .

# Equations when we have viscous fluids

When there is no viscosity the stress is of the form

$$\sigma = -pl.$$

When we have and incompressible Newtonian fluid with viscosity  $\mu \neq 0$  we have instead

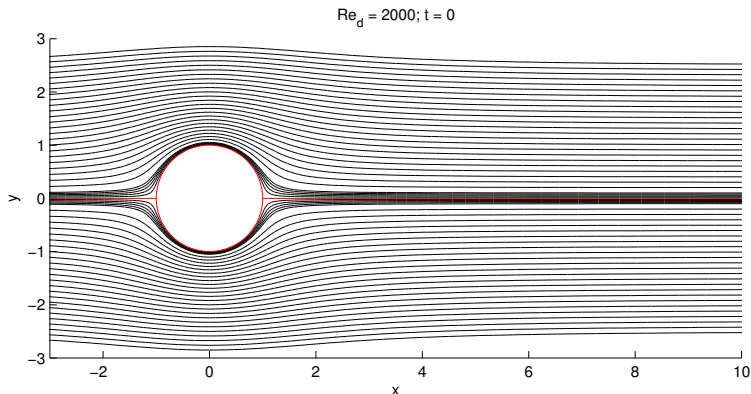
$$\sigma = -pl + \mu \begin{pmatrix} 2\frac{\partial u}{\partial x} & \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} & \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} \\ \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} & 2\frac{\partial v}{\partial y} & \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} \\ \frac{\partial u}{\partial z} + \frac{\partial w}{\partial x} & \frac{\partial v}{\partial z} + \frac{\partial w}{\partial y} & 2\frac{\partial w}{\partial z} \end{pmatrix}.$$

The equations of motion that this leads to are known as the Navier Stokes' equations. The following plots were obtained by approximately solving these equations using a Matlab program available from the URL: [http://www.cfmbyexample.com/resources/Cylinder\\_06October2011.zip](http://www.cfmbyexample.com/resources/Cylinder_06October2011.zip)



## Flow around a cylinder – inviscid case, $\mu = 0$

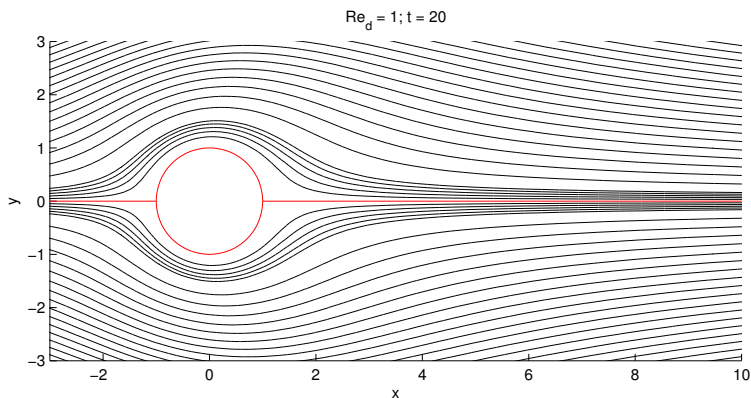
There is frictionless flow around the cylinder. The streamlines for this case are given in the next chapter of the notes.



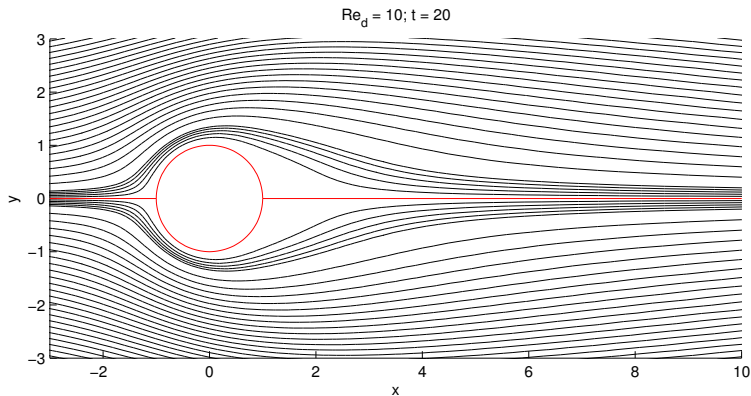
# Flow around a cylinder – Reynold's number, $Re=1$

No fluid has no viscosity. The flow depends on something known as the Reynold's number where

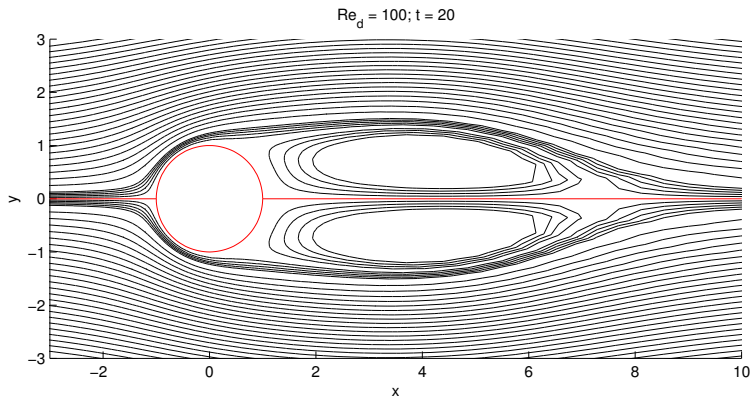
$$Re \propto \frac{|\text{inertia terms in equation of motion}|}{|\text{viscous terms in equation of motion}|}.$$



# Flow around a cylinder – $Re=10$



## Flow around a cylinder – $Re=100$



An inviscid model is not adequate in this case.